

Inter-modal interactions in a chain of mass-in-mass non-linear oscillators

J. Flosi^{*}, A. Ture Savadkoobi^{*}, C.-H. Lamarque^{*}

^{*} Univ Lyon, ENTPE, Ecole Centrale de Lyon, CNRS, LTDS, UMR5513, 69518 Vaulx-en-Velin, France



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Presentation of the system
Primary treatments

Asymptotic approach using multiple-scale

Analytical methodology

Results

Chain around mode 1 and 3
Experiment

Conclusion



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Systems for vibro-acoustical control

Linear systems (example: TMD¹) :

- ▶ Efficient on a narrow band of frequencies
- ▶ Modify system characteristics

Design and introduction of non-linearity² (example: nonlinear energy sink³) :

- ▶ Efficient on wider bands of frequency

Design and exploit nonlinearities in metamaterials

¹Frahm, 1911

²Roberson, 1952

³Vakakis et Gendelman, 2001

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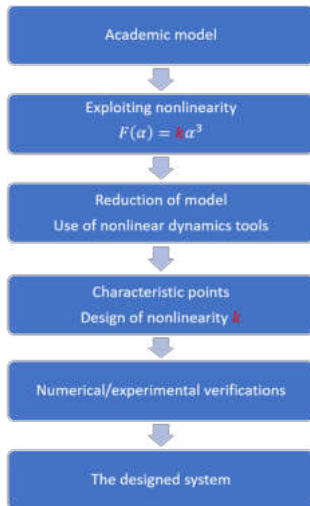
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General methodology



Continuous approximation of the chain

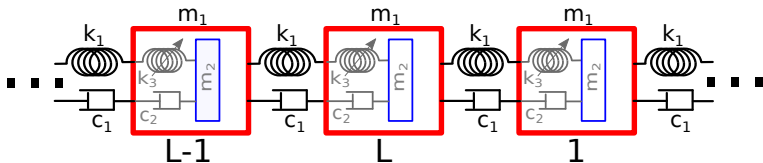


Figure: L-periodic chain composed by cubic nonlinear mass-in-mass cells

$$\begin{cases} \frac{\partial^2 U}{\partial \tau^2}(x, \tau) - \frac{\partial^2 U}{\partial x^2}(x, \tau) + \varepsilon \Lambda V^3(x, \tau) - \varepsilon \chi_1 \frac{\partial}{\partial \tau} \frac{\partial^2 U}{\partial x^2}(x, \tau) + \varepsilon \chi_2 \frac{\partial V}{\partial \tau}(x, \tau) = \varepsilon f(x, \tau) \\ \varepsilon \left(\frac{\partial^2 (U - V)}{\partial \tau^2}(x, \tau) - \Lambda V^3(x, \tau) - \chi_2 \frac{\partial V}{\partial \tau}(x, \tau) \right) = 0 \quad \text{with } x \in [0 : L] \end{cases}$$

- ▶ $\varepsilon = \frac{m_2}{m_1} \ll 1$: mass ratio
- ▶ $\tau = \sqrt{k_1/m_1} t$: non-dimensional time variable
- ▶ $\varepsilon \Lambda = \frac{k_3}{k_1}$, $\varepsilon \chi_1 = \frac{c_1}{\sqrt{k_1 m_1}}$, $\varepsilon \chi_2 = \frac{c_2}{\sqrt{k_1 m_1}}$ and $\varepsilon f_j = \frac{F_j}{k_1}$

Dispersion equation

Linear conservative associated system:

$$\frac{\partial^2 U_I}{\partial \tau^2}(x, \tau) - \frac{\partial^2 U_I}{\partial x^2}(x, \tau) = 0$$

$$\frac{\partial^2 (U_I - V_I)}{\partial \tau^2}(x, \tau) = 0$$

Harmonic decomposition of periodic solutions:

$$U_I(x, \tau) = h_j(x)g_j(\tau)$$

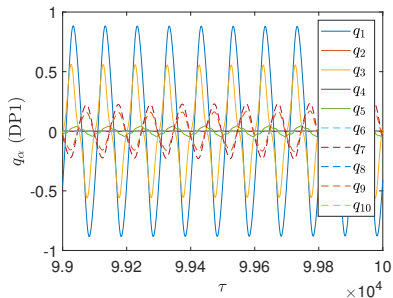
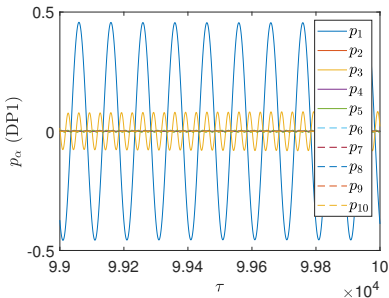
Expression of linear modes of the chain:

$$h_j(x) = \sqrt{\frac{2}{L}} \cos(\omega_j x + \theta_j)$$

$$\omega_j = \frac{2j\pi}{L}, \quad j = 1, \dots$$

Observation of modal exchanges due to non-linearity

Discrete system under first mode forcing associated to $f_1 = 0.004 \sin(\omega_1 \tau)$:



We investigate the $m : n$ inter-modal resonance ($m = 3n$) and define:

$$f(x, \tau) = f_n h_n(x) \sin(v_n \tau) + f_m h_m(x) \sin(v_m \tau)$$

$$v_j \approx \omega_j$$

$$U(x, \tau) = p_n(\tau) h_n(x) + p_m(\tau) h_m(x)$$

$$V(x, \tau) = q_n(\tau) h_n(x) + q_m(\tau) h_m(x)$$

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Complexification and harmonics selection

Projection of equations on internally resonant modes n and $m = kn$

Time decomposition in ε scale:

- ▶ fast time $\tau_0 = \tau$
- ▶ slow time $\tau_1 = \varepsilon \tau_0$

Introduction of Manevitch complex variables⁴ ($i^2 = -1$) around v_n and v_m :

- ▶ $\phi_n e^{i v_n \tau} = N_n e^{i \delta_n} e^{i v_n \tau} = \dot{p}_n + i v_n p_n$
- ▶ $\psi_n e^{i v_n \tau} = M_n e^{i \gamma_n} e^{i v_n \tau} = \dot{q}_n + i v_n q_n$
- ▶ $\phi_m e^{i v_m \tau} = N_m e^{i \delta_m} e^{i v_m \tau} = \dot{p}_m + i v_m p_m$
- ▶ $\psi_m e^{i v_m \tau} = M_m e^{i \gamma_m} e^{i v_m \tau} = \dot{q}_m + i v_m q_m$

Frequencies of external solicitations:

- ▶ $v_n = \omega_n + \varepsilon \sigma_n$
 - ▶ $v_m = \omega_m + \varepsilon \sigma_m = k v_n + \zeta_k \varepsilon$
- $$f = f_n h_n \sin(v_n \tau) + f_m h_m \sin(v_m \tau)$$

Implementation of Galerkin methodology (first harmonic v_n and k^{th} harmonic $k v_n$):

- ▶ $\frac{v_n}{2\pi} \int_0^{\frac{2\pi}{v_n}} s(\tau) e^{-i v_n \tau} d\tau$
- ▶ $\frac{v_n}{2\pi} \int_0^{\frac{2\pi}{v_n}} s(\tau) e^{-i k v_n \tau} d\tau$

⁴L. Manevitch, "The description of localized normal modes in a chain of nonlinear coupled oscillators using complex variables," Nonlinear Dynamics, vol. 25, pp. 95–109, 07 2001.

Complex equations

The system becomes:

$$\left\{ \begin{array}{l} \frac{\partial \phi_n}{\partial \tau_0} + \varepsilon \left(\frac{\partial \phi_n}{\partial \tau_1} + \mathcal{E}_n(f_n, \sigma_n, \phi_n, \psi_n, \psi_n^*, \psi_m, \psi_m^*) \right) = 0 \\ \frac{\partial \phi_m}{\partial \tau_0} + \varepsilon \left(\frac{\partial \phi_m}{\partial \tau_1} + \mathcal{E}_m(f_m, \sigma_n, \zeta_k, \phi_m, \psi_n, \psi_n^*, \psi_m, \psi_m^*) \right) = 0 \\ \frac{\partial \phi_n}{\partial \tau_0} - \frac{\partial \psi_n}{\partial \tau_0} + \mathcal{H}_n(\phi_n, \psi_n, \psi_n^*, \psi_m, \psi_m^*) = 0 \\ \frac{\partial \phi_m}{\partial \tau_0} - \frac{\partial \psi_m}{\partial \tau_0} + \mathcal{H}_m(\phi_m, \psi_n, \psi_n^*, \psi_m, \psi_m^*) = 0 \end{array} \right.$$

Fast time scale (ε^0):

- ▶ Detection of Slow Invariant Manifolds (SIMs)
- ▶ Stability of the SIM

Slow time scale (ε):

- ▶ Detection of singularities
- ▶ Detection of equilibrium points

Prediction of periodic and non-periodic behaviors

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Elements of the SIMs

System parameters: $\Lambda = 0.2$, $\chi_1 = 0.1$, $\chi_2 = 0.02$, $L = 100$

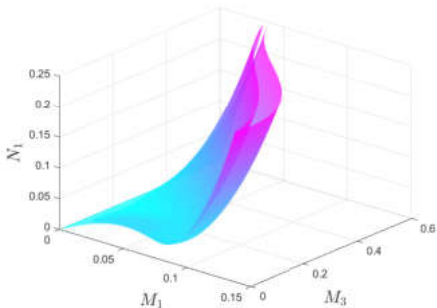


Figure: SIM envelopes around first mode ($\Gamma \in [0; 2\pi]$)

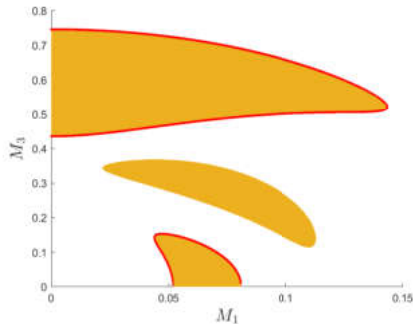


Figure: Unstable zone for $\Gamma = 3\gamma_1 - \gamma_3 = 0$

Free response of the system

Initial deformation on mode 1 $U(\tau = 0) = U_1 h_1(x)$

System parameters: $\varepsilon = 10^{-2}$, $\Lambda = 0.2$, $\chi_1 = 0.1$, $\chi_2 = 0.02$, $L = 100$

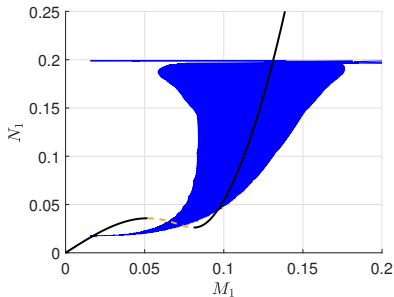


Figure: Free response on the 1 mode SIM

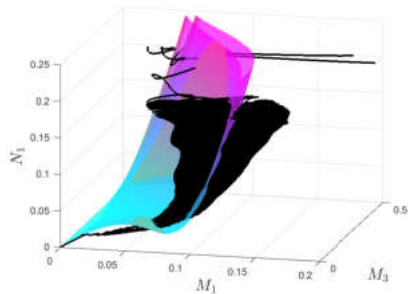


Figure: Free response on the 2 modes SIM

Chain around mode 1 and 3

Frequency response curves

System parameters: $\varepsilon = 10^{-2}$, $\Lambda = 0.2$, $\chi_1 = 0.1$, $\chi_2 = 0.02$, $L = 100$, $f_1 = 0.004$, $f_3 = 0$, $\eta_3 = 0$

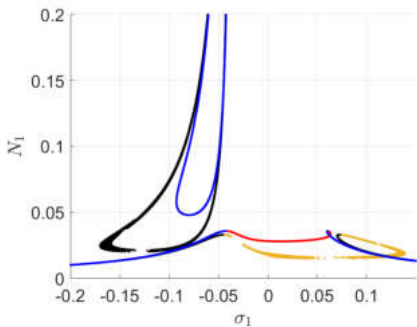


Figure: Frequency response curve according to mode 1

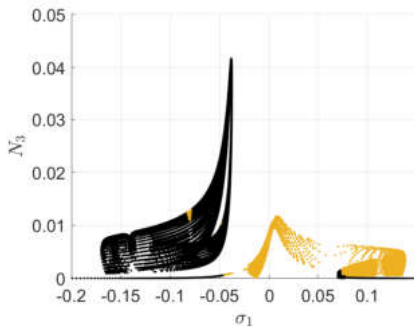


Figure: Frequency response curve according to mode 3

Chain around mode 1 and 3

Frequency response curves

System specs: $\varepsilon = 10^{-2}$, $\Lambda = 0.2$, $\chi_1 = 0.1$, $\chi_2 = 0.02$, $L = 100$, $f_1 = 0.004$, $f_3 = 0$, $\sigma_3 = 0$, $\sigma_1 = 0$

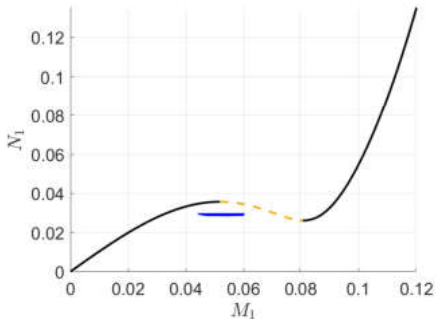


Figure: Frequency response curve according to mode 1

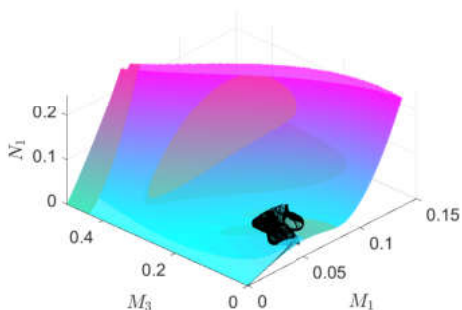


Figure: Frequency response curve according to mode 3

Example of application

System specs: $\varepsilon = 10^{-2}$, $\Lambda = 0.2$, $\chi_1 = 0.1$, $\chi_2 = 0.02$, $L = 100$, $f_1 = 0.004$, $f_3 = 0.024$, $\sigma_3 = -0.1$, $\Gamma \in [0; 2\pi]$

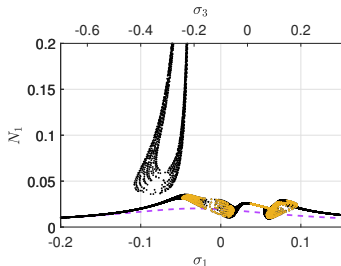


Figure: Frequency response curves according to mode 1

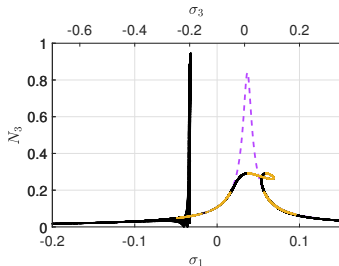


Figure: Frequency response curves according to mode 3

The experimental meta-cell

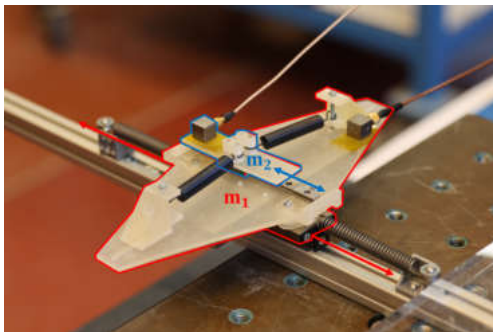


Figure: Experimental meta-cell

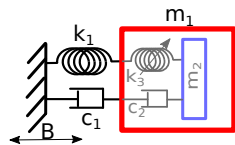


Figure: Theoretical meta-cell

specs: $k_1 = 2890 \text{ N.m}^{-1}$, $k_3 = 1,83 \cdot 10^5 \text{ N.m}^{-1}$, $m_1 = 0.814 \text{ kg}$, $m_2 = 0.026 \text{ kg}$, $c_1 = 1.47$, $c_2 = 0.17$.

Experiment on one cell

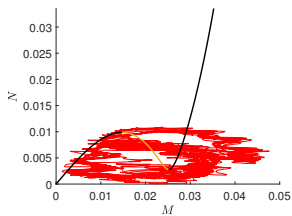


Figure: Experimental datas on the SIM for $B = 0.79$ mm and $f = 9.6$ Hz

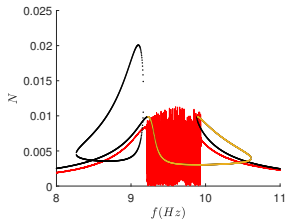
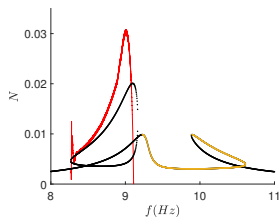


Figure: Experimental sweeps for $B = 0.79$ mm and $f \in [8 : 11]$ hz



Ongoing experiment on the non-periodic chain of 6 cells



Figure: Experimental mass-in-mass chain

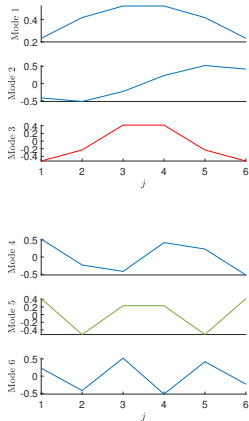


Figure: Modes of non-periodic chain

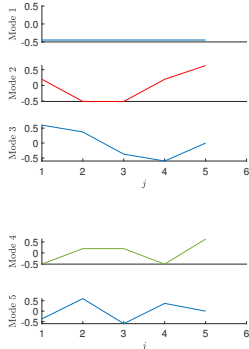
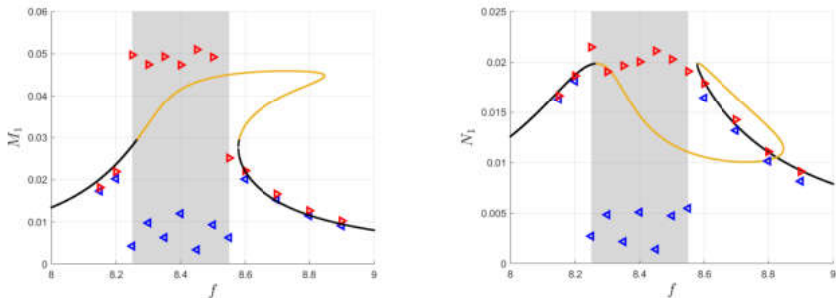


Figure: Modes of periodic chain

Ongoing experiment on the non-periodic chain of 6 cells

Figure: Experimental data collected for $B = 1.5$ mm



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Conclusion

- ▶ Fast dynamics: determination of the SIMs + several possible unstable zones
- ▶ Slow dynamics: Equilibrium and singular points (periodic and non-periodic responses)



Design tools for control or amplification of energy

Perspectives :

- ▶ Inclusion of more modal interactions (e.g. 3 modes)
- ▶ Experimental verification taking into consideration internal resonances